

1 **Prototype of alveolar gypsum blocks with plastic waste addition for partition** 2 **walls: Physico-mechanical, water-resistance and life cycle assessment**

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8 **Abstract**

9 The development of eco-friendlier building products incorporating waste as an alternative to raw materials has become
10 increasingly relevant within the construction industry. With this in mind, this study presents a prototype of an alveolar
11 gypsum block for partition walls, wherein partial replacement of the binder (i.e. gypsum or cement) was made using two
12 types of plastic waste (i.e. polypropylene- and nylon-based). Two plastic waste-containing composites, with contents
13 considered as optimum in previous studies (AGB/PP/7.5 - 7.5 wt% polypropylene content; AGB/PA6/2.5 - 2.5wt% nylon
14 content), were produced and extensively analysed in comparison to a reference block. Physico-mechanical (bulk density,
15 surface hardness, flexural and compressive strength), water permeability and thermal properties were evaluated and compared
16 to commercially available counterparts. In addition, the prototypes' environmental impact was determined by conducting a
17 simplified life cycle assessment primarily based on the “Global Warming Potential” and “Embodied Energy” categories. The
18 results showed a widespread improvement in the mechanical performance of plastic-containing blocks and more so for those
19 reinforced with nylon fibres when compared to the reference product. Furthermore, notable reductions in thermal conductivity
20 and water permeability were observed on the blocks due to the addition of plastic waste. Both types of blocks presented a
21 slight environmental impact decrease because of the reduction of raw materials (i.e. gypsum). These findings are encouraging
22 from a practical application point of view and may create a notable opportunity for replacing more frequently gypsum with
23 polypropylene- or nylon-based wastes for alveolar blocks for building partition walls.

24 **Keywords:** Polypropylene waste; nylon waste; gypsum block; physico-mechanical performance; life cycle assessment

26 **HIGHLIGHTS**

- 27 • Use of plastic waste to manufacture eco-friendly alveolar gypsum blocks
- 28 • Plastic waste-containing blocks showed improved mechanical performance
- 29 • Significant reduction in water permeability and thermal conductivity with plastic use
- 30 • Lower environmental impact was achieved due to the decreased use of raw materials
- 31

32 **ABBREVIATIONS LIST**

33 AGB - Alveolar gypsum block

34 CC - Coffee capsule

35 CoV - Coefficient of variation

36 CO₂ - Carbon dioxide

37 EE - Embodied energy

38 EPS - Expanded polystyrene

39 EU - European Union

40 FNs - Fishing nets

41 G - Gypsum

42 GWP - Global warming potential

43 HDPE - High-density polyethylene

44 ITZ - Interfacial transition zone

45 LCA - Life cycle assessment

46 LCI - Life cycle inventory

47 LCIA - Life cycle impact assessment

48 LDPE - Low-density polyethylene

49 LFS - Ladle furnace slags

50 PA - Polyamide

51 PA6 - Nylon

52 PC - Polycarbonate

53 PE - Polyethylene

54 PET - Polyethylene terephthalate

55 PP - Polypropylene

56 PUR - Polyurethane foam

57 W/G - Water/gypsum

58 XPS - Extruded polystyrene

59

60 1 INTRODUCTION

61 Climatic change is one of the most concerning environmental challenges currently being faced worldwide. Although many
62 efforts to tackle this widespread issue are exerted at a political level, such as the reduction of greenhouse gas emissions to
63 55% by 2030 (European Commission, 2020), an increase of alternative decarbonisation approaches in different industrial
64 sectors is needed. The construction industry stands as one of the main sectors that generate the highest negative impacts on
65 the environment since it is responsible for 39% of energy-related global carbon dioxide (CO₂) emissions, wherein 28%
66 comes from operational carbon and 11% arises from energy applied to produce construction materials (World Green
67 Building Council, 2019). Therefore, there is a considerable necessity for cross-sector coordination to revolutionise this
68 industry towards a net zero future, focused mostly on tackling the materials' embodied carbon and other adverse impacts
69 like dust/gas emissions, noise pollution, waste generation, water consumption, and air pollution (Dräger & Letmathe, 2022).
70 Such changes at the corporate level in construction are fundamental for the creation of more environmental-friendly
71 building materials, which have attracted a lot of attention from researchers in the construction field (Brahami et al., 2022;
72 Gangadhara et al., 2022; Zhang et al., 2022), capable of complying with European targets and the UN 2030 Agenda.

73 The generation of plastic waste, due to uncontrolled production and unsuitable waste management, has become one of the most
74 hazardous types of environmental pollution; over 57 million tonnes of plastic are produced annually in Europe while barely ~10%
75 of post-consumer plastic is recycled (Plastic Europe, 2022). This needs to be addressed by the different sectors involved (i.e.
76 production, using-life, disposal and waste treatment steps) to enhance materials' circularity, mainly the construction sector due to
77 its annual plastic consumption (around 22% of plastic produced at a European level) and wide-ranging relevance in the global
78 economy. An interesting solution would be extending the service life of construction systems by improving their properties or
79 developing new eco-friendly materials by using recycled wastes as a total or partial replacement for raw materials (i.e. gypsum,
80 cement, coarse, sand) (Gao et al., 2021,2023; Umar et al., 2021; Reshma et al., 2022).

81 There is a growing awareness of the production of new plastic waste-containing construction materials inserted in a circular
82 economy model, which leads to cost reductions, energy savings, and products with better performance (Manjunatha et al.,
83 2022; 2021a). The most sensible solutions offered by researchers within the construction sector to this problem have been:
84 replacing part of the natural aggregate fraction in concrete/asphalt production with plastic waste (Manjunatha et al., 2021b;
85 Thejaswi et al. 2023), using polymeric wastes as reinforcement fibres of concrete or gypsum/mortar composites (Reshma
86 et al., 2021; Manjunatha et al., 2021c) and partially replacing raw binder materials (i.e.. cement or gypsum) to produce new
87 products for building applications like plaster, bricks or precast panels and blocks (Adiyanto et al., 2022; Lamba et al.,
88 2022; Nyika & Dinka, 2022). Considering those structural materials must comply with strict standards to be used in

89 construction, most of those new products containing plastic waste are implemented as non-structural construction systems.

90 Interesting studies have been conducted on plastic-containing concrete and bitumen elements for pavement construction.

91 For example, Koppula et al. (2023) analysed the effect of a balanced mix containing high-density polyethylene (HDPE),

92 quartz sand, and bitumen to produce new lightweight pavement bricks, which showed reasonable strength and reduced

93 water absorption in comparison to conventional ones. The reinforcement of concrete pavement bricks by using waste plastic

94 fibres (i.e. nylon) was also explored by Yin et al. (2021). In this study, the optimal performance in bending strength and

95 water absorption corresponded to composites with a water/cement (w/c) ratio of 0.40 and waste fibre/cement addition ratio

96 of 1% by volume (v/v%), thus demonstrating the technical viability of using waste plastic fibres.

97 According to the literature, the development of building bricks by recycling plastic waste as sustainable construction materials

98 has attracted the attention of many researchers (Singh et al. 2023). Among them, the work conducted by Raj and Somasundaram

99 (2022) should be highlighted, wherein aerated concrete masonry blocks incorporating tyre waste powder (up to 15 wt%) as

100 replacement of fine aggregate were manufactured. The authors reported weight reduction, and an improvement in water

101 absorption, water permeability and sorptivity. Attending to the unsustainable waste management menace of E-waste plastics,

102 which are mainly landfilled or burned, Arya et al. (2023) presented a safe recycling proposal towards transforming obsolete

103 keyboard-based plastic into fine aggregate to produce concrete mixed with eggshells and fly ash for masonry blocks production

104 (EN 771-1 +A1, 2016). The highest comprehensive strength (~15 MPa) was obtained with the combination of 3.12%, 3.12%,

105 and 6.25%, relative to E-waste, eggshell, and fly ash, respectively, and thus the product could be classified as second-class brick.

106 Zulkernain et al. (2022) analysed the influence of using different types of plastics (i.e. PET, HDPE, LDPE, PP) as partial

107 replacement (up to 6 wt%) of sand in the manufacture of cement bricks. As a result, it was confirmed that the proposed

108 mathematical model developed can be used to predict the required hardened properties of plastic cement bricks, leading to

109 greater use of plastic waste in building materials. In addition, the combination of waste gypsum (i.e. wet flue gas

110 desulfurization - WFGD) and fly ash (0-40 wt% replacement level of WFGD) to produce composite blocks was studied by

111 Sithole et al. (2023). The mechanical performance significantly decreased with fly ash addition in comparison to reference

112 WFDG, due to the low pH of the binary mix and reduced pozzolanicity of fly ash incorporated. However, it was suitable

113 to prepare lightweight composite bricks that comply with the minimum compressive strength of 1.5 MPa set by standard

114 to be used in construction, by applying a curing temperature of 40 °C at a 20 wt% fly ash level of replacement.

115 The need to accelerate and standardise construction techniques to reduce cost, speed up time and minimize environmental impacts

116 has promoted the search for new products that allow precast and modular construction systems. With this in mind, gypsum

117 products have been progressively more implemented in practice due to their versatility, vast number of possible applications,

118 low-cost and relatively low-impact material, and adequate thermal and acoustic properties (Lushnikova and Dvorkin 2016).

119 Numerous research studies have been conducted on possible alternative recycled solutions for plastic waste as aggregate
120 for gypsum mixes to develop gypsum-based construction products. Pedreño-Rojas et al. (2020b) proposed eco-friendly
121 gypsum plates reinforced with CD and DVD residues. Polycarbonate (PC) waste was used as crushed aggregate in the
122 gypsum matrix, as full pieces into the plates (4 scenarios) or combining them. As a result, lighter plates (around 15%
123 decrease with 60 wt% PP content, in comparison to reference plate) with lower thermal conductivity values (around 0.16
124 W/(mK)) were obtained. It was found that the best mechanical performance was achieved by the combined use of both
125 reinforcement options, i.e. crushed aggregate and full pieces. Likewise, the use of plastic waste sourced from discarded
126 cables as a partial replacement of gypsum in the production of plasterboards was studied by Vidales-Barriguete et al.
127 (2021a; 2021b). These authors reported that the modulus of elasticity of the new material was enhanced by ~50%, leading
128 to a notable improvement in cracking and impact resistance, when compared to traditional boards. Replacement levels of
129 up to 50 wt% of cable waste were suitable to obtain adequate values of flexural strength within standard requirements.
130 Moreover, plasterboards' resulting roughness pointed to an increase in adherence with an eventual render.

131 Concurrently, innovative studies related to the proposal of eco-friendly gypsum blocks by incorporating different types of waste
132 as an alternative to traditional brick partition walls have been found in the literature. Among them, the research conducted by
133 Singh et al. (2023, 2022), wherein agricultural waste-based gypsum hollow blocks (600 mm × 300 mm × 150 mm) were produced
134 with a density of between 1070-730 kg/m³ after adding 0-15 wt% of rice straw-based fibres, should be highlighted. When
135 compared to the solid blocks, the compressive strength of the hollow blocks decreased by 20-50%, but the thermal and acoustic
136 insulation significantly increased. The load-carrying capacity of agro-waste hollow gypsum blocks at an elevated temperature of
137 800 °C was also studied, obtaining encouraging results: A1 non-framing material, according to Euroclass classification.

138 The design of gypsum-based prefabricated blocks was also explored by Santamaría-Vicario et al. (2022), who determined the
139 suitability of using gypsum mortars with waste mineral additions of ladle furnace slags (LFS) as raw material to manufacture
140 precast products. The most suitable content chosen after subjecting gypsum mortar mixes to physico-mechanical, thermal and
141 acoustic performance tests was a 60 v/v% addition of LFS. Similar to mortar specimens, the new solid blocks (340 × 200 × 50
142 mm³) presented a trend of decreasing compressive strength (~40% reduction, when compared to reference material).

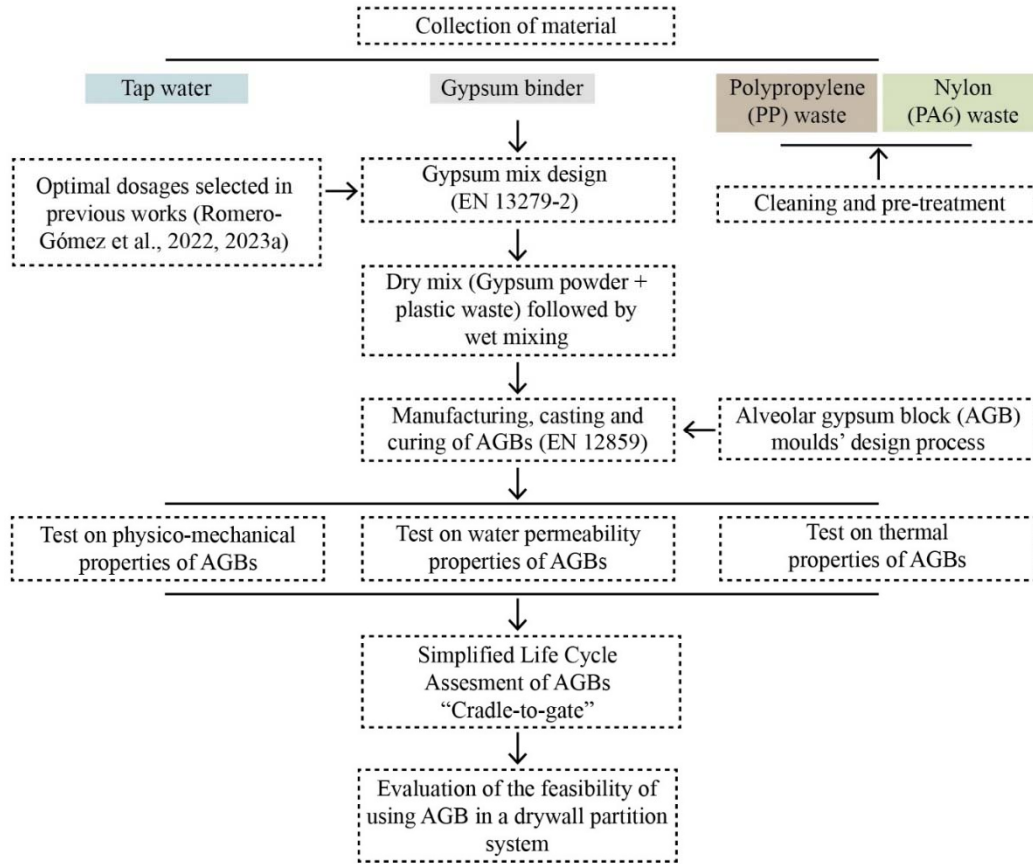
143 Villoria-Sáez et al. (2020) developed and tested a new hollow gypsum block (400 × 200 × 10 mm³) with a sandwich configuration.
144 The core of the block was filled with a gypsum mix (0.8 of water-to-gypsum ratio) incorporating 75 wt% of ceramic waste
145 addition and 2/3 v/v of EPS residue as partial replacement of the binder. Additionally, two laminated plasterboards (6 mm) were
146 placed in the outer layers. Although the new hollow blocks showed lower compressive strength when compared to the reference

147 solid block for traditional wall partitions, an improvement of up to 50% was reported in comparison to the reference non-sandwich
148 hollow blocks without waste additions. Moreover, Katman et al. (2022) found that the incorporation of optimized hollow cores
149 into gypsum blocks leads to better thermal and acoustic performance with minimized use of resources.

150 Because of the high rate of plastic production in relation to its deficient recyclability, the packaging and fishing sectors are
151 the two greatest contributors to environmental pollution. Most of their plastic wastes are dumped into landfills or incorrectly
152 disposed of directly into the environment, becoming sources of microplastic in marine ecosystems (80% of plastic waste
153 found in oceans comes from terrestrial activities and 20% from fishing works) (United Nations Environment Programme,
154 2021). After characterizing the nature of discarded products that are leaders in both sectors, polypropylene (PP),
155 polyethylene (PE) and polyamide (PA) should be highlighted and correctly managed. Despite the numerous market
156 opportunities offered by the properties of these types of plastic, like durability, strength, water resistance, and low thermal
157 conductivity properties, the circularity of post-consumer plastic waste is significantly low.

158 For these reasons, this research study focused on the use of two types of plastic, which are representative of the vast majority
159 of generated plastic waste, i.e. PP (from disposable coffee capsules - CCs) and PA (from fishing nets - FNs), for the
160 production of gypsum-based elements. In previous research (Romero-Gómez et al., 2022; 2023a), the authors evaluated
161 the feasibility of using both types of plastic waste (i.e. PA6 fibres and PP particles) as partial replacements for gypsum to
162 develop eco-friendly composites. In both cases, different replacement levels were analysed to ascertain the optimal mix
163 design. The optimization criterion followed consisted of seeking a maximum quantity of plastic waste that allowed for
164 improved or equal performance of the reference gypsum composite properties. Therefore, the main goal of the current
165 study is to evaluate the applicability of those gypsum composites (Romero-Gómez et al., 2022; 2023a), belonging to a
166 larger research project, to develop an environmental-friendly construction product for interior wall partitions. To this
167 purpose, two types of alveolar gypsum blocks (AGBs) were manufactured by incorporating 7.5 wt% of shredded PP waste
168 and 2.5 wt% of PA6 waste fibres, respectively. The experimental campaign consisted of three phases (Figure 1). Firstly,
169 the design and optimization of a block mould prototype were carried out. Secondly, the evaluation of physico-mechanical
170 (i.e. dry bulk density, superficial hardness, mechanical strength), water permeability and thermal properties of AGBs was
171 conducted in accordance with standard EN 12859 (2012). Also, a simplified life cycle assessment (LCA) of the products
172 was developed, in order to set a complete comparative analysis to determine the most feasible solution for wall partitions,
173 based on environmental, economic and physico-mechanical performance. Finally, a comparative analysis of commercial
174 and the proposed alveolar gypsum block prototypes was carried out in terms of physico-mechanical, thermal, and water-
175 resistant properties to establish the feasibility of developing those new solutions at an industrial level. The foremost novelty
176 of the aforementioned approach is the proposal of a research methodology to manufacture and evaluate the performance of

177 a gypsum-based prototype incorporating two types of highly pollutant plastic fractions. This study aims at minimizing the
 178 considerable challenges for the disposal of those residues while producing novel alveolar gypsum blocks with comparable
 179 physico-mechanical, water-resistant and environmental properties to those of commercial partition wall systems.



180
 181 Figure 1. Research methodology scheme of the current study.

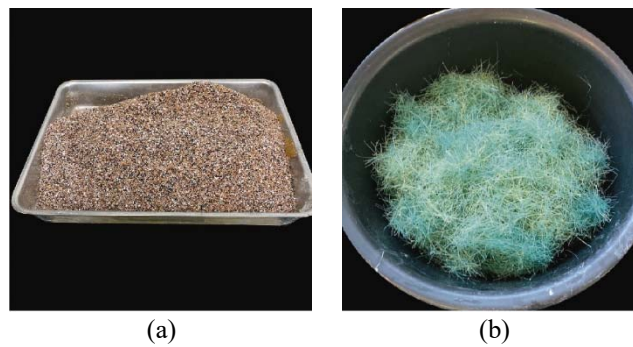
182 2 MATERIALS AND METHODS

183 2.1 Materials

184 To develop the current research, the following materials were used:

- 185 - Setting-controlled gypsum for construction (B1): purity > 75%, particle size range of 0-1 mm, surface hardness
- 186 Shore C < 45, flexural strength of 1 N/mm², compressive strength of 2 N/mm² and a pH > 6, may be highlighted
- 187 as the main properties, in accordance with standard EN 13279-2 (2009);
- 188 - Tap water, according to Council Directive 98/83/EC (1998);
- 189 - Polypropylene (PP) waste: shredded particles with an output size < 4 mm (Figure 2a) and a real density between
- 190 895-920 kg/m³. Main mechanical properties of PP particles: tensile strength - 29.5 ± 1.4 MPa; Young's modulus

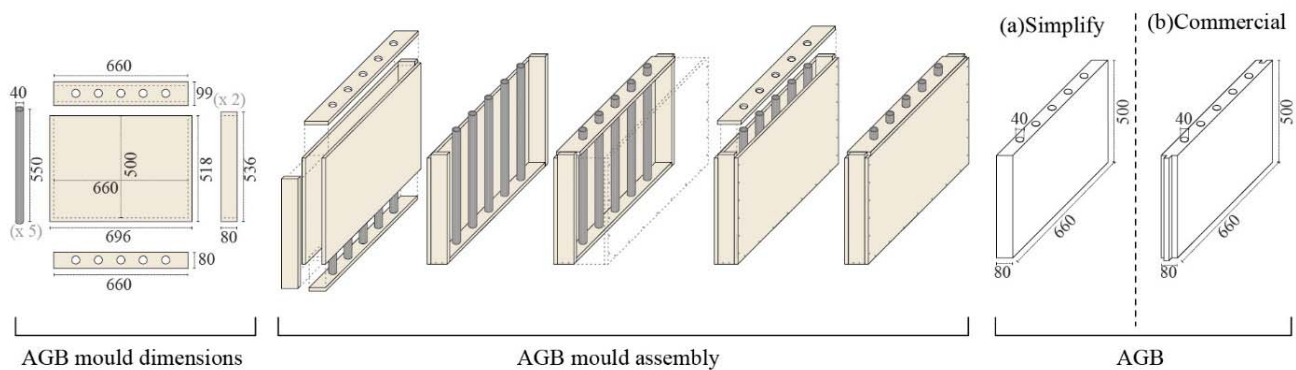
191 - 655 ± 9 MPa; yield point - 25.8 ± 1.5 MPa; ductility - 120.3 ± 20.6 %; toughness - 17.1 ± 2.9 J/m³; resilience
 192 toughness - 2.1 ± 0.7 J/m³ (Domingues et al., 2020). PP waste was sourced from disposable coffee capsules (CCs),
 193 subjected to cleaning and crushing processes using a RETSCH SM 2000 cutting mil. A density-based separation
 194 in water was used to recover each of the materials (i.e. PP and aluminium particles) to minimize contamination.
 195 Finally, PP granules were dried at 100 ± 2 °C until constant mass (Romero-Gómez et al, 2022);
 196 - Nylon (PA6) waste fibres: recycled monofilament fibres with 20-25 mm in length (Figure 2b), constant diameter
 197 of $\varnothing 240$ μ m and a real density of 1130 kg/m³. The main mechanical properties of PA6 fibres are: aspect ratio -
 198 L/D of 94; tensile strength - 440 MPa; Young's modulus - 3000 MPa; specific gravity - 1130 kg/m³ (Srimahachota
 199 et al., 2020). PA6 waste fibres were obtained from discarded fishing nets and underwent washing, air-drying and
 200 manual cutting procedures (Romero-Gómez et al., 2023a).



201 Figure 2. Plastic waste ready to be added to gypsum mix: a) PP particles; b) PA6 fibres

202 2.2 Alveolar gypsum block (AGB) moulds' design process

203 The design and manufacturing procedure of the AGB prototype is shown in Figure 3. The dimensions of the blocks (660
 204 mm in length \times 500 mm in height \times 80 mm in thickness) were established in accordance with standard EN 12859 (2012).
 205 Furthermore, the new blocks were carried out with a circular alveolar system of 40 mm in diameter. Pinewood was used
 206 as the main material of the mould. Five PVC tubes with 40 mm of external diameter were applied as negatives.



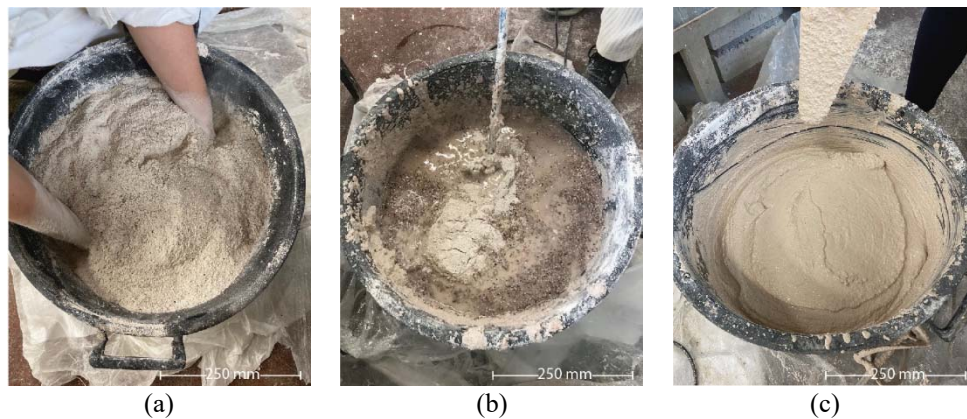
207 AGB mould dimensions
 208 AGB mould assembly
 208 AGB

208 Figure 3. Alveolar gypsum blocks (AGB) mould design, in mm

209 As seen in Figure 3, commercial AGBs typically have a tongue-and-groove system to facilitate and accelerate the construction
 210 process that does not influence the AGBs' physico-mechanical performance. Thus, the mould used to produce AGBs in this
 211 study was simplified, removing the tongue-and-groove, to facilitate their manufacturing for the experimental campaign.

212 2.3 Mix preparation and manufacturing of AGB prototypes

213 In the authors' previous works (Romero-Gómez et al., 2022; 2023a), specimens with several replacement levels of the same
 214 waste material were compared to understand the implications on the physico-mechanical performance of gypsum-based
 215 composites. This allowed defining the optimal replacement levels for each type of waste ((7.5 wt% PP waste particles and 2.5
 216 wt% PA6 recycled fibres, in weight of gypsum) that can effectively be used in practice whilst maintaining adequate
 217 performance for this specific application (i.e. alveolar gypsum blocks). Regardless of the type of waste incorporated into the
 218 gypsum mix, the same guidelines were followed to prepare all the samples (Figure 4). First, the waste (i.e. PP particles or PA6
 219 fibres) was dry-mixed with the gypsum powder to avoid the formation of waste agglomerations. After that, the water (0.55
 220 w/g ratio fixed for all mixes, determined as per standard EN 13279-2) was gradually added and all the components were mixed
 221 with a handheld electric mortar mixer for 2 min until a homogeneous state was reached. Three specimens were developed per
 222 type of plastic waste, including reference gypsum ones. The mix proportions by type of waste needed to prepare a block
 223 sample are summarized in Table 1. The mix code for the different samples is the following: alveolar gypsum block (AGB);
 224 type of waste used - polypropylene (PP)/nylon (PA6); percentage of plastic waste addition (e.g. AGB/PP/7.5).



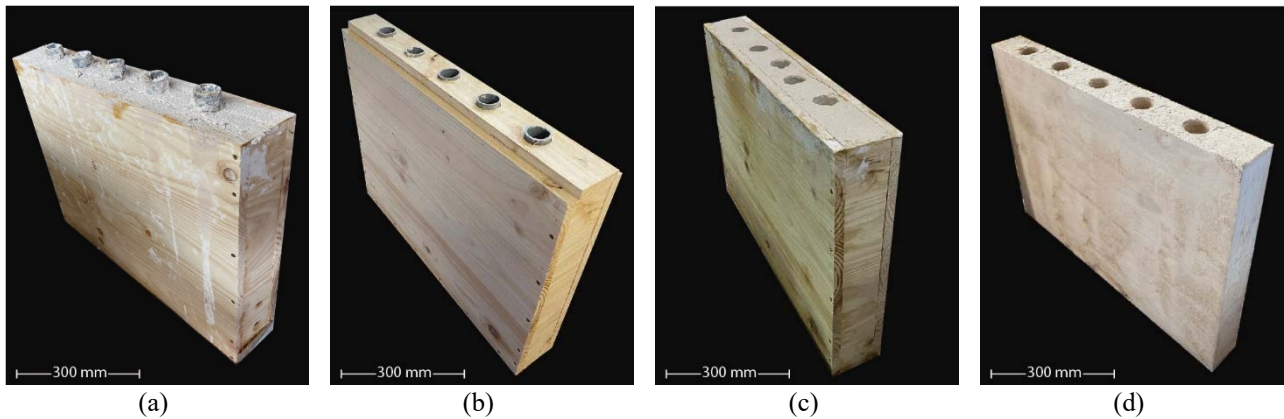
225 Figure 4. Samples preparation procedure: a) plastic waste-gypsum dry mixing; b) water incorporation and mixing for 2 min; c) mix
 226 ready to be moulded

227 Table 1. Mix proportions for an AGB specimen of 660 mm × 500 mm × 80 mm

Mix code	Gypsum [g]	Water [g]	W/G ratio	WasteWaste [g]	Waste [% v/v]
G/CM	30000	16500	0.55	-	-
G/PP/7.5	27750	15263	0.55	2250	17.2
G/PA6/2.5	29250	16089	0.55	750	4.96

228

229 After concluding the mixing procedure, the mix was then poured into the aforementioned wooden mould, previously coated
230 with a release agent. Subsequently, a top wood piece was placed in order to level the top surface of the AGB. After 1 h, the
231 PVC tubes were taken off. Finally, the AGB was removed from the mould after 24 h and placed in a dry chamber. The
232 steps described can be observed in Figure 5.



233 Figure 5. Moulding procedure to make an AGB: a) pouring of the mix into the mould; b) smoothing of the top surface; c) removal of
234 the cylindrical pieces; and d) AGB after demoulding

235 2.4 Curing conditions

236 Attending to the requirements set by standard EN 12859 (2012), after demoulding the AGBs, they were cured in a dry
237 chamber for 18 days, until constant mass. The conditions of the chamber were controlled to maintain a temperature of 23
238 ± 2 °C and relative humidity of 55-65%.

239 2.5 Test methods

240 2.5.1 Physico-mechanical properties

241 - *Dry bulk density*: this property was calculated according to the procedure set by standard EN 12859 (2012), based on the
242 relationship between the dry weight and volume of the block samples. The final value of dry bulk density was determined
243 by the arithmetic mean of the three samples measured per AGB type.

244 - *Superficial hardness (Shore C)*: prior to a destructive mechanical test, this method was developed according to standard
245 12859 (2012). To this purpose, each test piece (660 mm \times 500 mm \times 80 mm) was placed on a horizontal and flat surface
246 where the superficial hardness was measured by a durometer Shore C (Figure 6a). Twelve measurements were made per
247 surface. The final value was obtained as the arithmetic mean of the highest ten recorded values by the group. Three samples
248 by AGB type were analysed.

249 - *Flexural strength*: determined by the flexural breaking load of the panels (660 mm \times 500 mm \times 80 mm) subjected to the
250 three-point method included in standard EN 12859 (2012). The test piece was placed between two parallel cylindrical

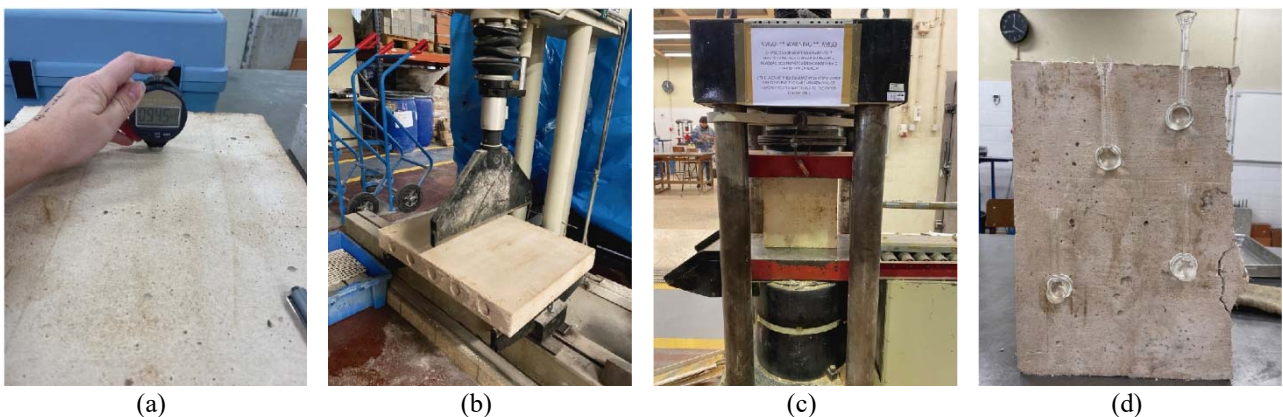
251 supports separated by 566 mm (Figure 6b). Then, a continuous load of 20 N/s was applied in the central plain until the
252 block's failure. The flexural testing equipment Form+Test Seidner+Co GmbH D-7940 Riedlingen was applied. For each
253 of the AGB groups, the value of flexural strength was calculated as the arithmetic mean of the three specimens measured.
254 - *Compressive strength*: considering the absence of specific regulations to evaluate the gypsum blocks' compressive
255 strength, the guidelines established by standard EN 772-1+A1 (2011) for masonry units were followed. Pieces of 300 mm
256 × 300 mm × 80 mm were obtained from samples subjected to flexural test. The compression testing machine Form+Test
257 Seidner+Co GmbH MEGA 6-3000-100 was used to develop this test. Every piece was carefully aligned with the centre of
258 the plate. Then, a centred load was applied with a velocity of 0.05 (N/mm²)/s, until reaching the maximum load causing
259 failure (Figure 6c). Afterwards, the average value was calculated from three samples per AGB type.

260 2.5.2 Water permeability

261 - *Water absorption by pipe method*: this test consisted of measuring the amount of water (ml) transferred from the pipette
262 through a given test area (cm²) after a set time (20 min.), expressed in ml/cm², as per standard EN 16302 (2016). A
263 minimum of three measurement areas were taken by block sample (Figure 6d). The change in the water level in the
264 graduated column was noted at time intervals of 10-60 seconds. Subsequent measurements were registered every 5 min
265 until constant value (max 1 h). Three samples (half of the block resulting from flexural test ~330 mm × 500 mm × 80 mm)
266 by AGB type were analysed. The final value was established as the average value of nine measurements by the AGB group.

267 2.5.3 Thermal performance

268 - *Thermal conductivity test*: following the guidelines set by standard ASTM D5930-17 (2009), the thermal conductivity
269 coefficient of three cylindrical samples (Ø60mm /e = 20 mm) per type of mix, was measured by using the ISOMET 2114
270 equipment connected to a surface probe. The dynamic measurement method was around 30 min per measurement.



271 Figure 6. Tests developed: a) superficial hardness (Shore C); b) flexural strength; c) compressive strength; d) water permeability under
272 low pressure.

273 2.5.4 Simplified Life Cycle Assessment

274 A simplified comparative life cycle assessment (LCA) was conducted, using a “cradle-to-gate” model to evaluate the
275 environmental impacts of the proposed plastic waste-containing AGBs for use in partition walls. This was done in accordance
276 with previous works, which classified this methodology as the most efficient to evaluate the environmental impact of a
277 construction material (Pedreño-Rojas et al., 2019a; Zabalza-Bribián et al., 2011). The aim of this analysis is to determine
278 whether the environmental suitability of PP- and PA6-containing AGBs outweigh any performance shortcomings and thus
279 discern the validity of their implementation in practice. Therefore, the environmental impacts of each AGB were obtained as
280 follows: identification and quantification of the different materials used to develop the new products, related to the
281 requirements set by standard EN 15804 (2014), modules from A1 to A3 “Product stage”, raw material supply, transport and
282 manufacturing processes were considered; application of the LCA methodology in order to obtain the environmental impact
283 of each AGB type - “cradle-to-gate” model.

284 Goals and scope

285 Embodied Energy (EE [MJ]) and Global Warming Potential (GWP [kg CO₂eq.]) were identified as the most relevant impact
286 indicators to be applied in LCA for building applications, according to previous research (Pedreño-Rojas et al., 2019b; Omar,
287 2018; Soust-Verdaguer et al., 2016; Suárez et al., 2016). The impact assessment was conducted following the methodology
288 described by García-Martínez (2010). EcoInvent v3.0 (EcoInvent Association, 2013) and ITEC (ITEC Database, 2023) as
289 LCA databases, as well as manufacturers' information related to equipment efficiency, were used for this analysis.

290 The functional unit chosen in this work is 1 m² of each type of AGB partition wall, having different amounts of gypsum, plastic
291 waste (i.e. PP or PA6) and water. As shown in Figure 7, the system boundary for the process considers three different phases:

- 292 - Raw material supply: it includes all the processes to obtain the different materials needed to develop the new
293 composites (commercial gypsum, recycled plastic waste (i.e. PP and PA6) and water);
- 294 - Transportation: it makes reference to the transport of each material from the quarry and recycled plant to the
295 product factory;
- 296 - Product manufacture: it covers all the mixing, moulding, curing and packaging procedures to get the new AGBs.

297 Life cycle inventory (LCI) and life cycle impact assessment (LCIA)

298 The LCI of the production of each material involved in the manufacturing process to obtain each type of AGB was
299 calculated by applying the following steps:

- 300 - Identification of the processes and materials that were needed to develop the gypsum-based mixes. All the phases

301 to obtain commercial gypsum (B1) were considered, according to published information (Pedreño-Rojas et al.,
 302 2020a). Furthermore, the washing, shredding and drying procedures used by recycling companies to obtain PP
 303 and PA6 waste ready to be incorporated into the gypsum mixes were evaluated. However, plastic waste
 304 management phases were rejected for the LCA assessment (landfilling, incineration, etc.), as suggested by studies
 305 from the literature (Goyal et al., 2023; Pedreño-Rojas et al., 2019b; Nyland et al., 2003), since these are 'final use'
 306 or 'end-of-life' phase for materials. So, recycling was the only phase that was considered;

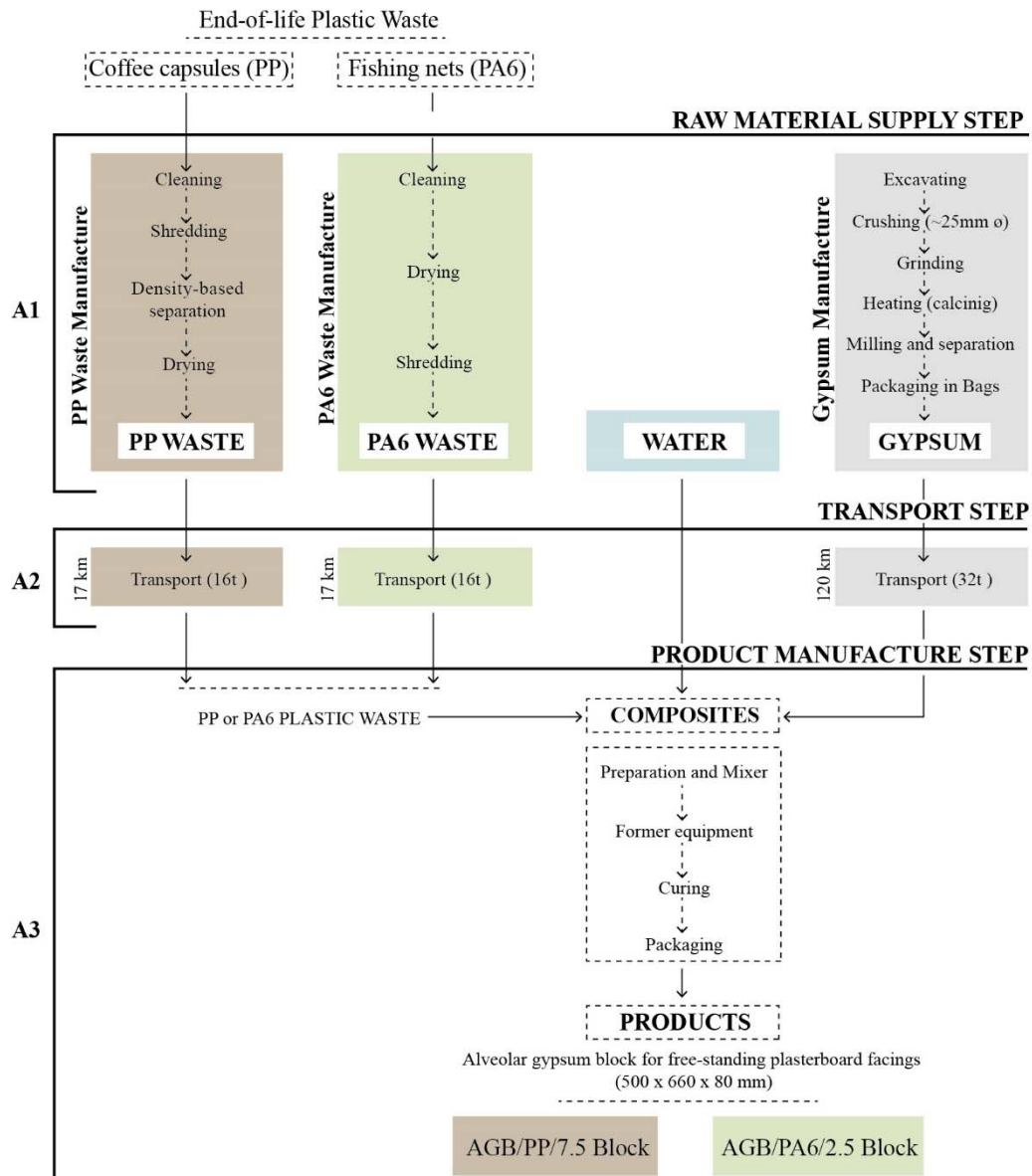


Figure 7. System boundary for the LCA of manufacturing the alveolar gypsum-PP/PA6 blocks.

307
 308 - Transport quantification. The means of transport used to bring each material from the gypsum extraction and
 309 production or the recycling plant (i.e. PP and PA6 waste) to the gypsum block factory, as well as the distance
 310 travelled, were considered;

- 311 - Inventory of product manufacture procedure. In this case, all the equipment involved in the production of AGB
 312 was considered: mixer machine to obtain gypsum-based composites, formwork equipment to mould AGB, curing
 313 chamber and packaging equipment to get the AGB ready to be commercialised. These processes were the same
 314 for all the mixes with the exception that a 2 min plastic waste-gypsum powder dry mixing stage was needed for
 315 the plastic waste previously to water addition, and therefore considered;
- 316 - Determination of the environmental impact of each unit procedure. The impact values of each unit process were
 317 sourced from EcoInvent v3.0 (EcoInvent Association, 2013) and ITEC (ITEC Database, 2023) databases;
- 318 - Assessment. To obtain the LCIA of the complete procedure, GWP and EE impacts were calculated.

319 Table 2 summarizes the amount of each material, energy and transport required to produce a square meter (m²) of each
 320 gypsum-based block. In addition, Table 3 shows an inventory of the equipment used with their corresponding power
 321 consumption per ton of material to produce the different types of AGB. Finally, a list of the extracted data for each material
 322 and procedure included in the LCIA of the products under study is exposed in Table 4.

323 Table 2. Amount of raw materials required to produce a square meter [m²] of AGB partition wall

Material used	Unit	Reference material	G/PP/7.5	G/PA6/2.5
Gypsum	kg	90	83.2	87.7
Water	kg	49.5	45.8	48.2
PP waste	kg	-	6.8	-
PA6 waste	kg	-	-	2.3
Electricity	kWh	-	12.5	7.5
Transport 16-32 t	tkm	120	120	120
Transport 7.5-16 t	tkm	-	17	17

324

325 3 RESULTS AND DISCUSSION

326 Concluding the evaluation of physico-mechanical, water-resistance and thermal properties of the proposed alveolar gypsum
 327 blocks containing PP and PA6 residues, the results are summarized and discussed in this section. Next, the environmental
 328 impact of the new products after reducing the raw material (i.e. gypsum) use by incorporating plastic waste, was evaluated.
 329 Finally, the practical feasibility analysis of the new AGBs was carried out, in comparison with similar commercial solutions.

330 3.1 Physico-mechanical properties

331 3.1.1 Dry bulk density

332 Concerning the dry bulk density values obtained from each type of AGB shown in Figure 8, a slight increase in density can
 333 be observed in the plastic waste-containing AGB. After incorporating PP waste particles into the gypsum mix, the resulting
 334 blocks presented a rise of up to 2.3%, while the addition of PA6 waste fibres led to an increase of ~5%. Although the raw
 335 material (i.e. gypsum) with a density of 2300 kg/m³ was partially replaced by plastic waste (i.e. PP and PA6) with low

336 density (895 kg/m³ and 1130 kg/m³, respectively) for the production of AGB, contrary to expectations, lighter materials
 337 were not obtained. Similar findings were reported previously (Romero-Gómez et al., 2022; 2023a) in small-scale
 338 composites (40 × 40 × 160 mm³), the data of which can be consulted in Table 5.

339 Table 3. Inventory of equipment used and energy consumption per ton of material for the production of AGB partition walls

Component	Name in database	Reference source	Power type	Unit	Energy consumption per tonne	
Gypsum raw materials	Gypsum extraction		Diesel	l	5.56	
	Crushing		Electricity	kWh	32.61	
	Calcination	-	Natural gas	m ³	29.59	
	Milling and separation		Electricity	kWh	14.85	
	Packaging and storage		Electricity	kWh	11.23	
PP and PA6 waste	Washing, shredding and drying facilities	Washing system for thermoplastics	SIKOPLAST (SIKOPLAST Recycling Technology GmbH)	Electricity	kWh	20
PP waste	Density-based waste separation	Centrifuge separator for plastic recycling	TECNOFER (Tecnofer Recycling plants, machines and equipment for waste treatment)	Electricity	kWh	55
	Drying equipment	-	Pedreño-Rojas et al. (2019b)	Electricity	kWh	0.35
AGB manufacture	Mixer	Horizontal gypsum mixing machine	Yinda Machinery (YINDA Machinery)	Electricity	kWh	0.8
	Former equipment	Gypsum hollow block-making machine	Longkou Deyi Machinery Co., Ltd (DEYI group)	Electricity	kWh	2.78
	Curing	Gypsum blocks tunnel dryer	Münstermann (Thermoprozesstechnik, Handlingsysteme, Luftreinhaltung, Automatisierung - MÜNSTERMANN)	Electricity	kWh	1.11
	Packaging equipment	Gypsum blocks packaging machine	Matthys group (Matthys group, Innovative and customized machinery solutions)	Electricity	kWh	0.02

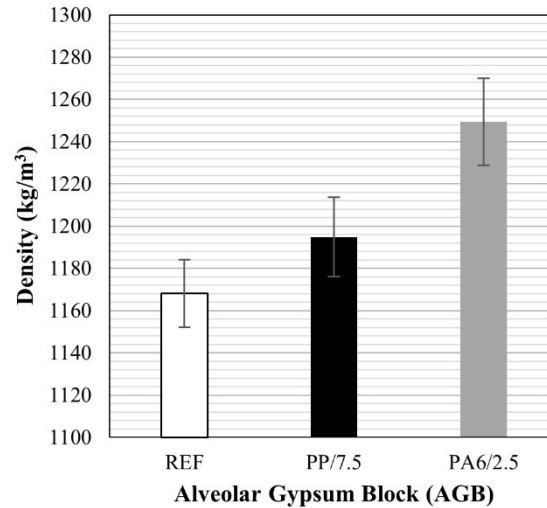
340
 341 Table 4. Materials used and their name in EcoInvent v3 (EcoInvent Association, 2013) and ITEC (ITEC Database, 2023) databases.

342 Unit values for Global Warming Potential and Embodied Energy

Component	ID	Name in database	Database	Unit	GWP (kg CO ₂ eq.)	EE (MJ)
Gypsum	B0521100	B1/20/2 Gypsum according to EN 13279-1	ITEC	kg	0.16	1.80
Water	2288	Tap water, at user	EcoInvent	kg	0.01	0.01
Electricity (plastic recycling)	698	Electricity mix, Spain (construction)	EcoInvent	kWh	0.50	10.9
Transport 7.5-16t	7301	Transport, lorry 7.5e16t, EURO4	EcoInvent	tkm	0.26	4.33
Transport 16-32t	7304	Transport, lorry 16-32t, EURO4	EcoInvent	tkm	0.15	2.58

343
 344 The incorporation of 7.5 wt% PP particles and 2.5 wt% PA6 fibres led to a densification of the gypsum matrix, more
 345 noticeable in the latter, due to the more extensive particle size distribution of the combined materials and reasonable

346 adhesion at the interfacial transition zone between waste aggregate-matrix. The superficial roughness of the waste
347 aggregate was a key factor in facilitating the gypsum crystal growth throughout the plastic waste's surface, especially
348 noticeable for PP particles.



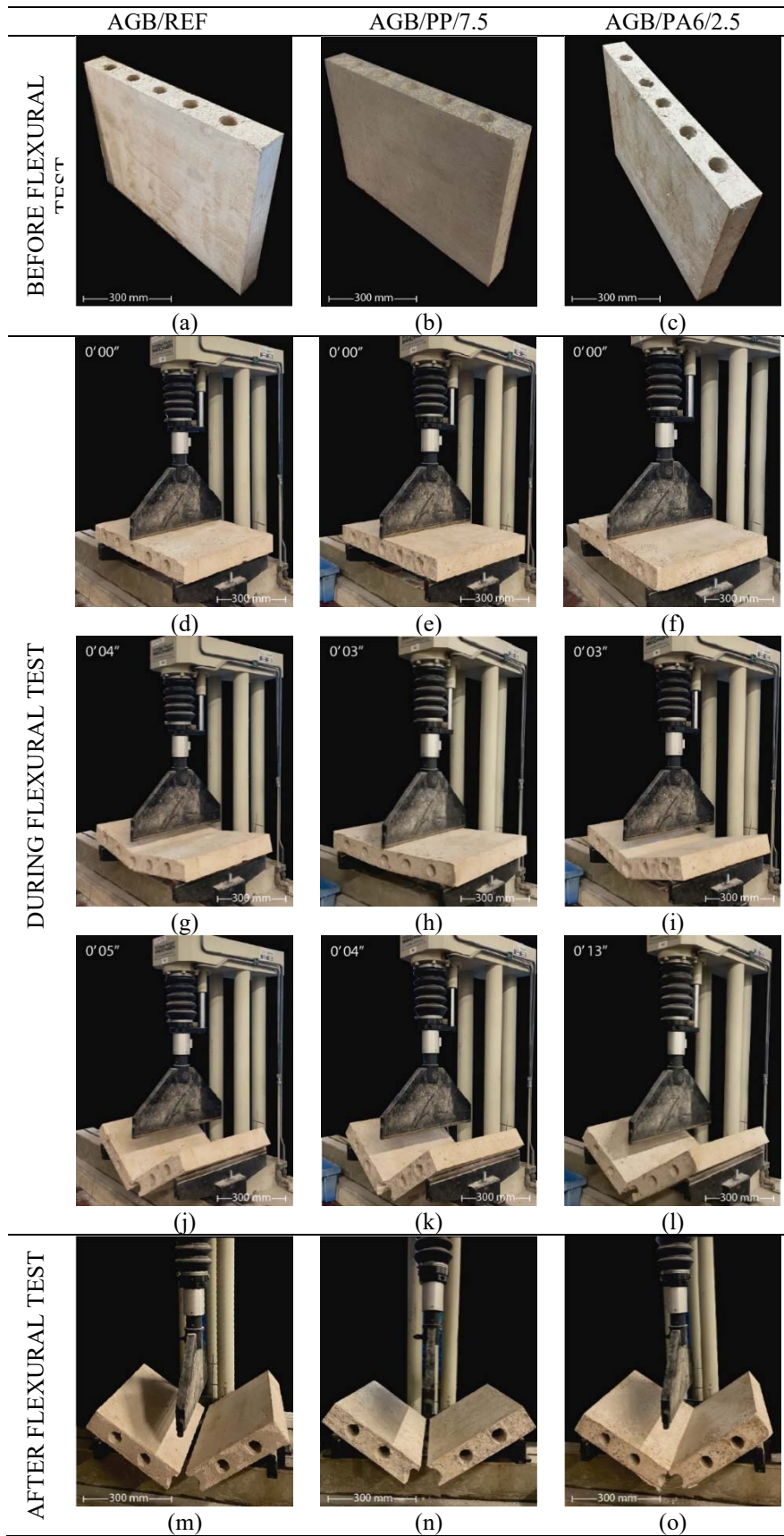
349 Figure 8. Dry bulk density values of the AGBs

350 3.1.2 Superficial hardness (Shore C)

351 The data obtained from the superficial hardness (Shore C) test: 95.6, 95.8 and 95.1, corresponding to G/REF, G/PP/7.5 and
352 G/PA6/2.5, respectively, pointed out that the addition of plastic waste to gypsum matrix did not influence the AGBs'
353 superficial hardness. In addition, all gypsum-based blocks could be classified as high-density blocks, since all the values
354 of superficial harness (Shore C) were over the minimum 80 Shore C units (2012).

355 3.1.3 Flexural strength

356 The three-point flexural test setup can be seen in Figure 9 as well as the failure dynamics over time. In Figure 10a, the
357 values of flexural strength obtained from each type of AGB are presented. The addition of PA6 fibres with a replacement
358 ratio of 2.5 wt% led to an improvement of ~8% in flexural strength, while the use of 7.5 wt% PP replacement led to a
359 reduction of this property of 6.5% when compared to the control AGB/REF. Based on previous studies by the authors
360 (Romero-Gómez et al., 2022; 2023a), both wastes were dispersed uniformly within the gypsum matrix and this difference
361 in performance could be explained by the high aspect ratio and high tensile strength of PA6 fibres in comparison to PP
362 particles. Nevertheless, all the values were well over the minimum value of 1.7 kN set by the standard (EN 12859, 2012).
363 Furthermore, the addition of PA6 waste fibres significantly increases the toughness of the material (Romero-Gómez et al.,
364 2023a) and prevents complete breakage of the AGB after being subjected to the flexural strength test, as seen in Figure 7.
365 In AGB/PA6/2.5 blocks, the aspect ratio of PA6 fibres was a key factor in keeping together the resulting pieces of the
366 blocks after breaking point, unlike AGB/PP/7.5 and AGB/REF, which presented a brittle failure, breaking completely.



367

Figure 9. AGBs before, during and after being subjected to the flexural strength test: a), d), g), j), m) AGB/REF; b), e), h), k), n)

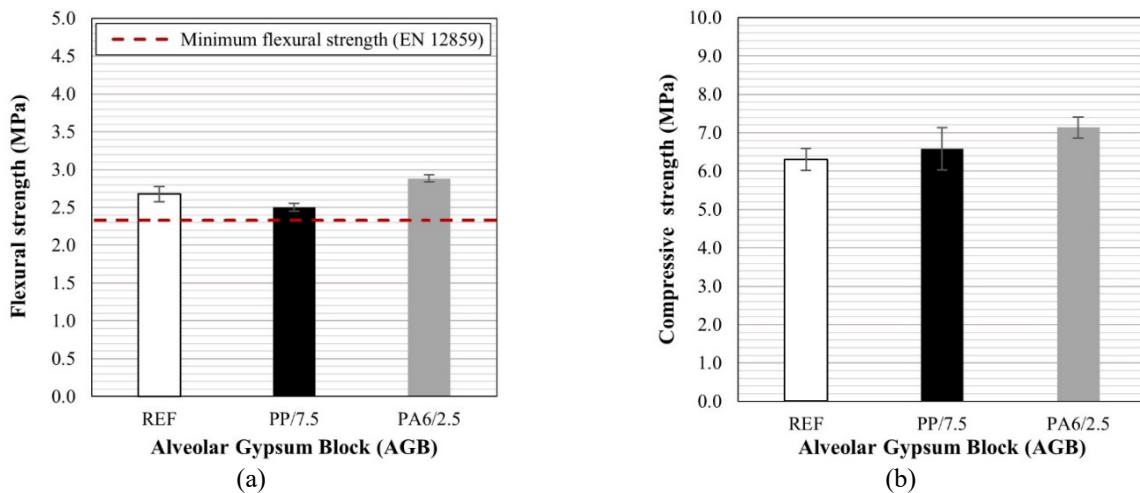
368

AGB/PP/7.5; c), f), j), l), o) AGB/PA6/2.5

369 Similar performance was observed previously by the authors when lower-scale composites containing recycled nylon fibres
 370 were subjected to flexural strength tests. After comparing two types of fibre size, it was concluded that longer ones
 371 prevented the complete destruction of the piece since they allowed for a more ductile behaviour as a result of their greater
 372 anchorage length, which gave rise to higher pull-out resistance (Romero-Gómez et al., 2023a), The research carried out by
 373 Yin (2021) and Orasutthikul et al. (2016) also concurred.

374 3.1.4 Compressive strength

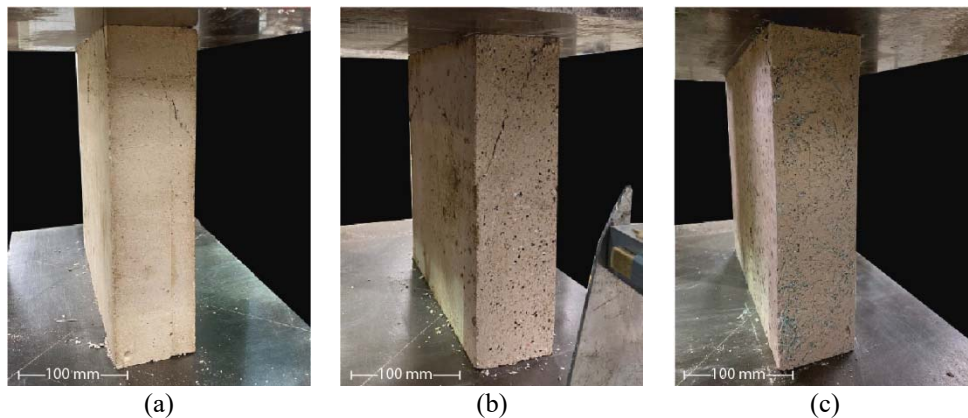
375 Figure 10b presents the compressive strength results of the different gypsum blocks. As expected, the compressive strength
 376 improved with plastic incorporation, due to the densification of the gypsum matrix observed in section 3.1.1 and verified
 377 by SEM analysis. The highest value was presented by AGB/PA6/2.5 (7.13 MPa), showing an increase of up to 8.4% with
 378 respect to the reference product. Similarly, the addition of PP also led to an increase in compressive strength of ~4.5%,
 379 when compared to AGB/REF. However, it must be noted that the enhanced values of compressive strength related mainly
 380 to PP waste-containing blocks are not significantly higher than those of the reference blocks, considering the overlapping
 381 standard deviation. In addition, a similar diagonal fracture line can be observed in Figure 11 in both AGB/REF and
 382 AGB/PP/7.5 specimens. The addition of PA6 fibres seems to have reduced the presence of such external cracks and instead
 383 induced linear cracks collinear in the loading direction.



384 Figure 10. Mechanical strength data of the AGB: a) flexural strength; b) compressive strength

385 The possible effects derived from scale change between gypsum plaster composites, previously studied by the authors
 386 (Romero-Gómez et al., 2022; 2023a), and the gypsum-based blocks were evaluated in this section. In general, a similar
 387 performance was detected in the materials in both studies (Table 5); G/PA6/2.5 and AGB/PA6/2.5 specimens showed the
 388 highest density values, superficial hardness and compressive strength. However, significant differences in flexural and
 389 compressive mechanical strength values were detected when comparing both scales for each corresponding mix.
 390 Reductions of 21% and 11% in flexural strength, and 18% and 15% in compressive strength, corresponding to AGB/REF,

391 and AGB/PA6/2.5, respectively, were registered. However, the change of scale did not seem to have an influence on
 392 flexural strength with the incorporation of PP particles, but rather on the compressive strength, since a reduction of up to
 393 21% was detected related to gypsum blocks when compared to smaller composites. Therefore, it can be observed that there
 394 was a lower difference in flexural strength values, related to the scale of the samples when plastic waste was added to the
 395 gypsum mixes. However, similar reductions of 15-21% were registered in blocks' compressive strength independently of
 396 the use of plastic waste as a partial replacement of the gypsum matrix. This fact pointed out that the creation of boreholes
 397 with 40 mm of diameter in the gypsum block prototype negatively affected the mechanical strength performance of the
 398 new products, especially compressive strength, at block scale (660 mm × 500 mm × 80 mm), due to the reduction of load
 399 application section thickness, as was previously observed by Villoria-Sález et al. (2020).



400 Figure 11. AGBs after being subjected to the compressive strength test: a) AGB/REF; b) AGB/PP/7.5; c) AGB/PA6/2.5



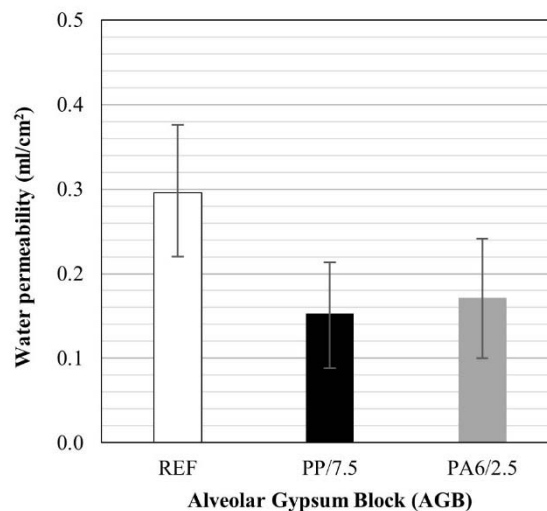
401 Figure 12. SEM analysis of: a) AGB/REF (400×); b) AGB/PP/7.5 (400×); c) AGB/PA6/2.5 (400×)

402 Table 5. Summary of the values obtained from physico-mechanical tests. Scale comparison between prismatic samples (40 mm × 40
 403 mm × 160 mm) previously analysed by authors [29], [30] and AGB (660 mm × 500 mm × 80 mm)

Sample code	Density (kg/m ³)	Superficial hardness (Shore C)	Flexural strength (MPa)	Compressive strength (MPa)
G/REF	1201.1	94.5	3.39	7.71
G/PP/7.5	1236.4	95.3	2.48	8.36
G/PA6/2.5	1228.4	97.3	3.26	8.35
AGB/REF	1168.0	95.6	2.68	6.30
AGB/PP/7.5	1194.8	95.1	2.50	6.58
AGB/PA6/2.5	1249.3	95.8	2.90	7.13

404 3.2 Water permeability

405 The data of the water permeability test are presented in **Error! Reference source not found.** Encouraging results were shown
406 by gypsum-based blocks containing plastic waste as the water permeability was reduced by 48% when compared to the
407 reference gypsum block. Although the lowest value (0.15 ml/cm²) corresponded to AGB/PP/7.5 specimens, a significant
408 decrease (of 42%) was also shown by AGB/PA6/2.5 specimens. Thus, the incorporation of impermeable plastic waste (i.e. PP
409 and PA6), as well as the densification derived from the incorporation of both types of plastic wastes as partial replacement of
410 the gypsum matrix did not induce a porous ITZ (Romero-Gómez et al., 2022; 2023a), leading to an improvement of the
411 gypsum block impervious property, which is one of the main handicaps of using gypsum products without additional
412 waterproofing treatments.



413 Figure 13. Values of water permeability of the AGBs

414 3.3 Thermal conductivity

415 The values of thermal conductivity coefficients obtained for AGB/REF, AGB/PP/7.5 and AGB/PA6/2.5 blocks were 0.39, 0.32
416 and 0.33 W/mK, respectively. The incorporation of plastic waste led to lower thermal conductivity coefficients when compared
417 to the reference product. Considering that the lowest value corresponded to 7.5 wt% PP-containing gypsum blocks, which means
418 a higher replacement level of plastic waste when compared to those containing 2.5 wt% PA6 fibres, a greater influence of the
419 replacement level can be inferred on thermal properties of gypsum products rather than the type of plastic. The decrement of the
420 thermal conductivity coefficients of the plastic waste-containing gypsum matrix can be attributed to the lower conductivity of the
421 plastic components (PP-0.22 W/(mK); PA6-0.25 W/(mK)), in comparison to the hydrated gypsum (0.39 W/(mK)). These data
422 are in accordance with the previous studies developed by Pedreño-Rojas et al. (2020c) and Vidales-Barriguete et al. (2018).

423 **3.4 Simplified Life Cycle Assessment**

424 As per Figure 14, a comparison of the GWP and EE of the studied AGBs was carried out. Regardless of the type of plastic
425 used as a partial substitute for gypsum, enhanced environmental benefits in terms of energy consumption (MJ ep.) and
426 GWP (CO₂ eq.) were observed for the proposed plastic-containing AGBs with respect to the reference one. AGB/PP/7.5
427 showed the highest global reduction in GWP and EE (~6% and ~3.5%, respectively) when compared to AGB/REF. PA6
428 fibre-containing blocks led to a reduction of ~2.5% in GWP and ~2% in EE in comparison to the reference AGB, which is
429 not as noticeable as the PP waste-containing blocks, because of the lower percentage of plastic waste used.

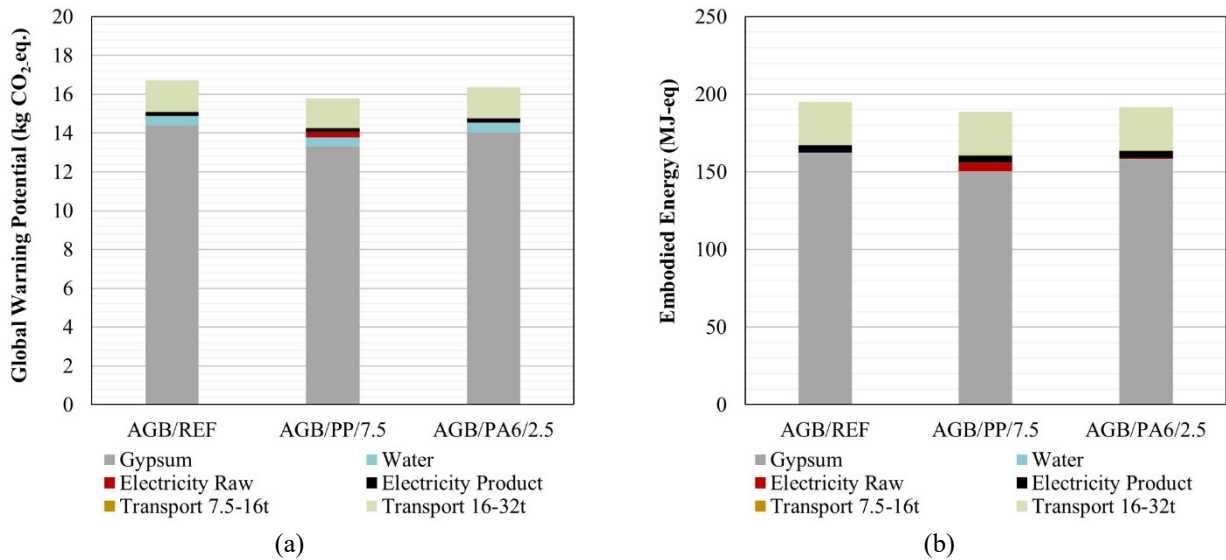
430 Comparing the graphs of both impact factors, a similar performance can be observed. The highest environmental impacts of
431 the AGBs were registered for the raw material supply phase. This phase corresponds to the whole process needed to obtain
432 the commercial gypsum in comparison to the minimum impact of the plastic waste washing and shredding procedure.
433 Nevertheless, the greater number of pre-treatment procedures required to obtain PP waste aggregate, in comparison to those
434 needed to get PA6 waste fibres, led to a higher electricity energy consumption. Thus, an increase of environmental impact
435 factors (i.e. GWP and EE) corresponding to the raw material supply phase of AGB/PP/7.5 blocks was detected, which partially
436 counteracted the environmental impact reduction achieved by the partial replacement of commercial gypsum by PP waste. In
437 spite of this, the global environmental impact of PP-/PA6-containing gypsum blocks corresponding to this first phase (i.e. raw
438 material supply) was lower than that of the reference AGB. On the other hand, the environmental impacts of the transportation
439 step were similar in all cases, since, as the amount of commercial gypsum transport decreased, the transport of recycled plastic
440 increased. In addition, it must be noted that the values of the GWP and EE impact factors were the same for the product
441 manufacture step since there were no modifications to the procedures conducted in this phase for the different mixes.

442 Summing up, in Figure 14, the input that contributes the most to the environmental impacts of the proposed gypsum-based
443 products is “Gypsum material”. Therefore, further research lines could be focused on the substitution of commercial gypsum
444 for a recycled one and/or increasing the percentage of plastic waste content, by assuming the loss of mechanical strength
445 within the minimum established in the standards (Goyal et al., 2023; Pedreño-Rojas et al., 2020a; 2019b; Sáez et al., 2020).

446 **3.5 Evaluation of the feasibility of using AGB in a drywall partition system**

447 The proposed prefabricated element (i.e. AGB) is a self-supporting construction system for interior partitions that can
448 represent an alternative option for the traditional ceramic system (i.e. double hollow brick). Some of the main features of
449 the AGB system include quick installation, easy assembly, no time-consuming plastering work, lightweight, non-
450 combustibility, toughness, as well as, enhanced thermal due to the hollow core system, thus making it a cost-effective and
451 sustainable solution that should be increasingly commercialized.

452 The current work proposes two alternative eco-friendly AGBs for drywall partition systems based on a standardized and
 453 commercialized building system. In order to evaluate the viability of both products in relation to the current commercial
 454 solutions, a comparative analysis between the main physico-mechanical properties of new plastic-waste-containing AGBs
 455 and several commercial solutions was carried out (Table 6). Gypsum blocks with hollow cores and other solid blocks were
 456 chosen to conduct this comparative assessment.



457 Figure 14. Life cycle impact assessment: a) Global Warming Potential (GWP) (kg CO₂ eq.); b) Embodied Energy (EE) (MJ eq.), refers
 458 to a functional unit of each type of AGB

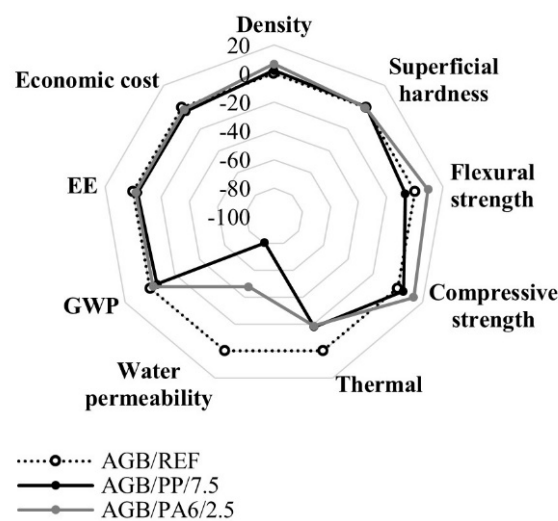
459 Table 6. Comparison of physico-mechanical properties of the new plastic waste-containing AGBs proposed in this work with respect to
 460 different alveolar and solid gypsum blocks available in the market with similar performance

Brand code	Type of block*	Dimension (mm)	Mass per m ² (kg/m ²)	Density class** (kg/m ³)	Superficial hardness (Shore C)	Flexural strength (kN)	Fire reaction	λ (W/(mK))	Water absorption (%)
AGB/PP/7.5	Alveolar (5T)	666/500/80	89 ± 1	D	95	1.8	A2	0.32	H3, no requirement
AGB/PA6/2.5	Alveolar (5T)	666/500/80	93 ± 1	D	96	1.9	A2	0.33	H3, no requirement
VOLMA80	Alveolar (9L)	667/500/80	90 ± 1	D	≥ 80	≤ 1.7	A1	0.35	H3, no requirement
MultiGips M80	Solid	500/500/80	114 ± 1	D	≥ 80	≥ 5.7	A1	-	H3, no requirement
Isolava Isomur	Solid	666/501/80	76 ± 1	M	≥ 55	≥ 2.7	A1	0.32	H3, no requirement
Alba hydro 80	Solid	666/501/80	80 ± 1	M	≥ 55	≥ 2.7	A1	0.58	H3, no requirement

461 *Type of block: Alveolar (5T - five boreholes in the transversal direction; 9L - nine boreholes in the longitudinal direction)
 462 **Density class: D (Dense); M (medium)

463 Firstly, attending to the mass per square meter corresponding to each solution, AGB/PP/7.5 and AGB/PA6/2.5 presented
 464 similar values to perforated commercial blocks also classified as Dense (D) class (e.g. VOLMA80), according to standard
 465 EN 12859 (2012). However, it should be highlighted that a decrease of 22% in weight is possible in the systems containing

466 plastic waste (corresponding to AGB/PP/7.5) presented here when compared to solid dense blocks (i.e. MultiGips M80)
 467 due to the hollow core. Nevertheless, this alveolar system leads to a reduction of around 67% in flexural strength in PP-
 468 and PA6-containing AGBs, when compared to solid dense gypsum-based blocks and ~30% related to solid medium-dense
 469 blocks. Even so, both types of the proposed AGBs presented values over the minimum set by the standard (1.7 kN) and
 470 were similar to commercial perforated blocks (e.g. VOLMA80). In addition, the proposed AGBs were better in terms of
 471 superficial hardness (highest values of Shore C) when compared to standard solutions; up to 20% and 75% increase related
 472 to commercial D and medium (M) class blocks, respectively. This is likely to reduce any visible superficial defects from
 473 the use of the surrounding area. Moreover, in accordance with previous studies by the authors (Romero-Gómez et al.,
 474 2023b), it is already known that the AGB containing PA6 waste fibres and those with PP residue particles can be considered
 475 as non-combustible products, classified as A2 Euroclass fire reaction. Furthermore, a decrease in thermal conductivity (up
 476 to 8.5%) was verified because of the partial replacement of gypsum with plastic waste, when compared to commercial
 477 alveolar blocks thereby making it a more cost-effective solution to maintain user comfort during the building's service life.
 478 Concerning the materials' water absorption, no requirements are needed for the new and commercial blocks since they are
 479 classified as H3 (> 5% of water absorption). In sum, the feasibility of manufacturing and applying the new AGBs proposed
 480 in this work as an interior wall partition system has been demonstrated since both of the proposed plastic waste-containing
 481 solutions can offer similar or even improved physico-mechanical and thermal performance to currently commercialized
 482 solutions. A summarized visual comparative assessment of the physico-mechanical, thermal and environmental properties of
 483 both types of AGBs proposed in this work (i.e. AGB/PP/7.5 and AGB/PA6/2.5), in relation to reference alveolar blocks
 484 without plastic addition, is shown in Figure 15.



485

486

Figure 15. Visual comparative analysis of the physical-mechanical, thermal and environmental properties of the AGBs

487 It can be inferred that AGBs reinforced with 2.5 wt% of PA6 waste fibres presented the best overall performance. Although a
488 slight increase in density was detected, this led to a notable improvement in flexural and compressive strengths. Furthermore,
489 a notable reduction in thermal conductivity was achieved. Even though the highest reduction of water permeability absorption
490 corresponded to AGB/PP/7.5 blocks, AGB/PA6/2.5 showed reduced water absorption capacity by 48%, with respect to the
491 reference, offering a solution to one of the main handicaps of using gypsum products without a water-repellent treatment.
492 Finally, from an environmental perspective, slight reductions in pollutant impact factors (i.e. EE and GPW), as well as in
493 economic costs, were achieved, associated with the low percentage of plastic waste used. Nevertheless, further reduction is
494 possible, which opens more research lines focusing on the optimization of physico-mechanical enhancements and
495 environmental-economic benefits by increasing plastic waste replacement levels.

496 **4 CONCLUSIONS**

497 Normalized alveolar gypsum block prototypes with dimensions of 660 mm × 500 mm × 80 mm were developed by
498 incorporating PP and PA6 waste as partial replacements of gypsum. The physico-mechanical, water permeability and
499 thermal performance of both types of blocks were analysed and compared to the reference material, thus allowing the
500 following conclusions:

- 501 - The incorporation of plastic waste led to an increase in the gypsum-based blocks' density because of the matrix's
502 enhanced compactness. Consequently, the compressive strength of both plastic waste-containing prototypes increased,
503 though more noticeably in the AGB/PA6/2.5 blocks with an 8.4% increase relative to the reference material;
- 504 - Regarding flexural strength, significant enhancement was also observed after using 2.5 wt% PA6 waste fibres as a
505 partial replacement of the binder (~8% increase when compared to AGB/REF). Although the incorporation of PP
506 waste led to a slight reduction in the block's flexural strength, all values were over the minimum set by the standard;
- 507 - The use of a hollow core system led to a reduction in mechanical performance, regardless of the plastic content,
508 when compared to lower-scale solid composites previously studied by the authors;
- 509 - A notable reduction in water permeability was detected in blocks containing plastic waste. The largest decrease
510 in water permeability was achieved by AGB/PP/7.5 blocks (~42%) because of the matrix' densification and the
511 PP's impervious nature. So, independently of the type of plastic used in this case, the water permeability decreases
512 depending on the amount of waterproofing material used, since both led to a reduced porosity at ITZ, contributing
513 to water absorption slowing down;

514 - Lower thermal conductivity coefficients were obtained with the use of plastic waste as gypsum replacement. The
515 thermal performance of alveolar gypsum blocks was best for those containing the highest amount of plastic (0.32
516 W/(mK) for 7.5% PP-containing blocks vs. 0.39 W/(mK) of the control blocks);

517 - Concerning the environmental impact assessment, the block prototypes showed slight enhancements in terms of
518 energy consumption and Global Warming Potential mainly due to the reduction of raw material use, when compared
519 to the reference product. Although a higher amount of waste was added to AGB/PP/7.5 blocks, the need for greater
520 pre-treatment of the waste gave rise to similar values of environmental impact factor in AGB/PA6/2.5 blocks.

521 Therefore, it was confirmed that both types of the proposed plastic-containing alveolar gypsum blocks could be applied as
522 elements in wall partition systems in building applications since they offered similar performance to that of current
523 commercial solutions. In terms of physico-mechanical performance, better results were obtained in ABG/PA6/2.5 blocks,
524 while AGB/PP/7.5 offered better water resistance and thermal behaviour, as well as lower environmental impacts. Thus,
525 considering that both solutions complied with standard regulations, they could be used as substitutes for conventional
526 partition systems, reducing construction costs, time and environmental pollution.

527 Finally, considering the limitations of the proposed methodology, the use of relatively low replacement levels of plastic
528 waste must be highlighted. This can be justified by the need to maintain the workability of the material without resorting
529 to the use of water-reducing admixtures and avoid impacting the mechanical performance significantly when compared to
530 the control product. Naturally, this led to little improved environmental performance. Moreover, given the results of the
531 simplified LCA, a relatively high impact related to the pre-treatment of plastic waste (mainly PP) was observed even for
532 the low levels of replacement evaluated here. Therefore, future research must focus on increasing plastic residue content
533 subjected to less impacting treatment processes, despite the potential decline in performance. Such an approach is viable
534 from an optimization perspective since the blocks proposed in the present study were well over the minimum strength
535 requirements set by standards. This would lead to a further decrease in environmental impacts and an improvement in
536 thermal and water-resistant behaviours. Naturally, a more complete LCA could also be developed considering a greater
537 number of impact categories, with the purpose of offering a complete environmental characterization of the new products
538 in comparison with commercial solutions.

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545 **Declaration of competing interest**

546 The authors declare that they have no conflict of interest.

547 **Credit authorship contribution statement**

548 **M.I. Romero-Gómez:** Methodology, Investigation, Writing - original draft, Writing - review & editing

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550 **J. de Brito:** Writing - review & editing, Analysis of results.

551 **I. Flores-Colen:** Writing - review & editing, Analysis of results, Supervision.

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